

# **MATHEMATICAL ANALYSIS OF ASTM-96 BASED TEWL CALIBRATION METHOD**

R E Imhof<sup>1,2</sup>, M E P de Jesus<sup>3</sup>, P Xiao<sup>1,2</sup> and the TEWL Calibration Consortium<sup>4</sup>

*<sup>1</sup> Photophysics Research Centre, London South Bank University, London SE1 0AA, UK*

*<sup>2</sup> Biox Systems Ltd, Southwark Campus, 103 Borough Road, London SE1 0AA, UK*

*<sup>3</sup> Departamento de Fisica, Universidade da Beira Interior, 6200 Covilhã, Portugal*

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# Presentation Outline

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# Water Vapour Flux Density Calibration Methods

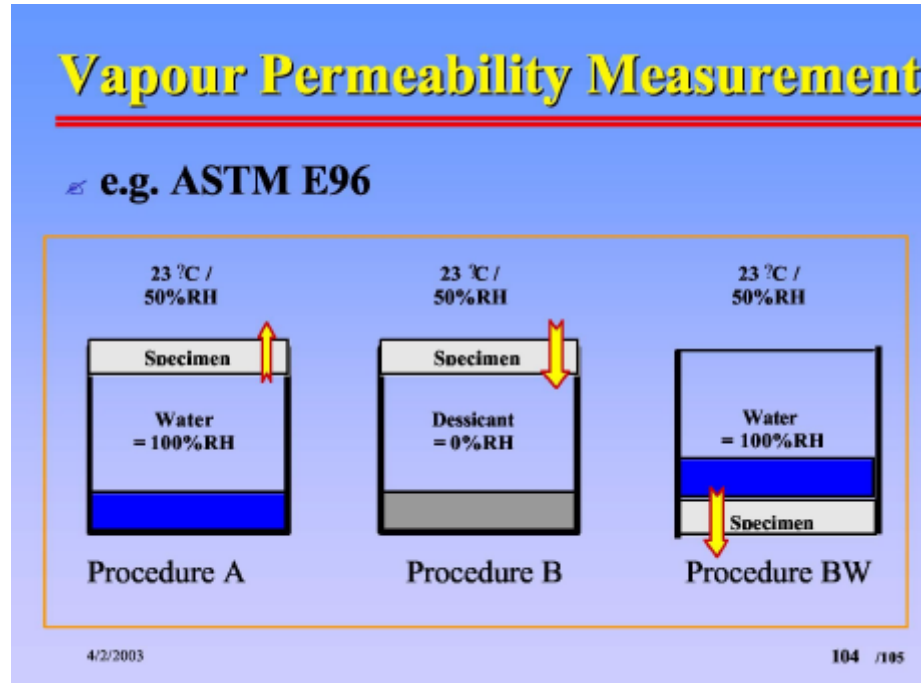
## **1. Membrane Methods**

Widely used. Broadly based on the ASTM-96 standard.

## **2. Water Droplet Method**

New approach, adopted when we discovered fundamental problems with the Membrane Method.

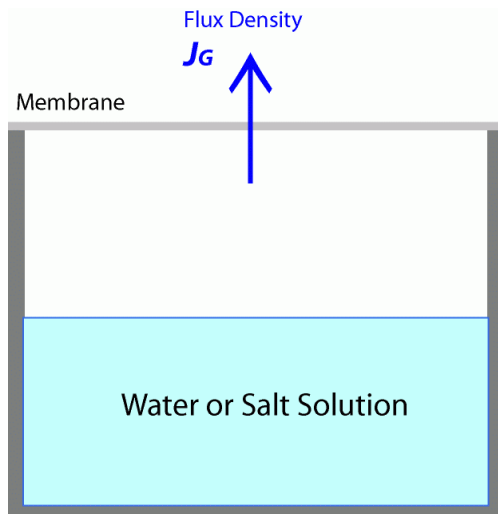
# ASTM-96 Summary



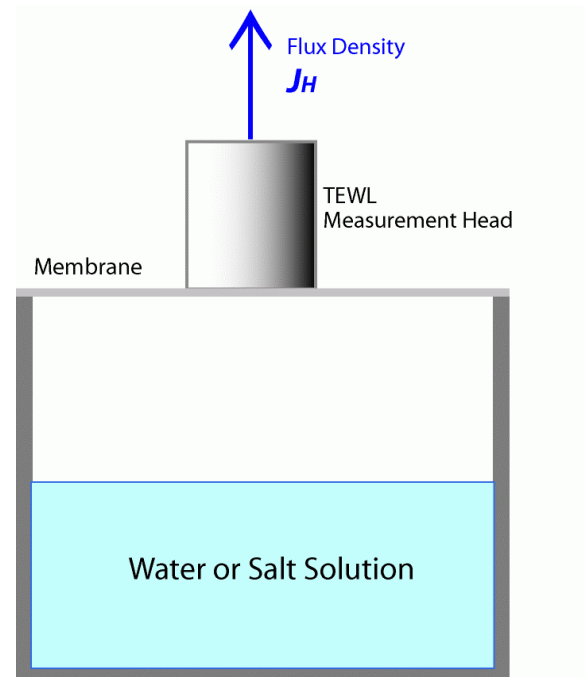
Reproduced from:- *Understanding Water: The Physics of Moisture Dynamics*. J Straube, University of Waterloo, Canada.

NB:- ASTM-96 was developed for characterizing membranes, NOT for calibrating TEWL.

## Membrane Method for TEWL Calibration



Gravimetric measurement of Flux Density  $J_G$ , from cup weight loss



Calibration of TEWL instrument, assuming  $J_H = J_G$

# Membrane TEWL Calibration - Example 1

Flux calibrated from weight loss of saturated salt solution.

Reservoir covered by a permeable membrane.

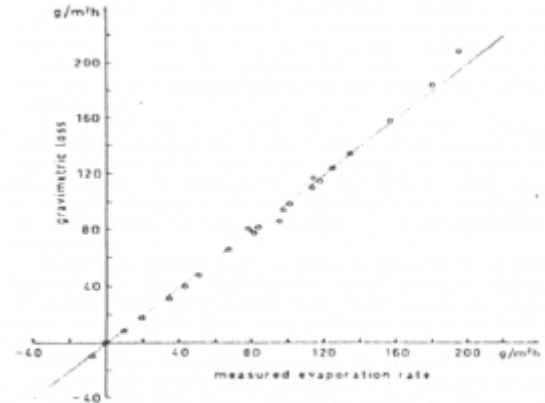
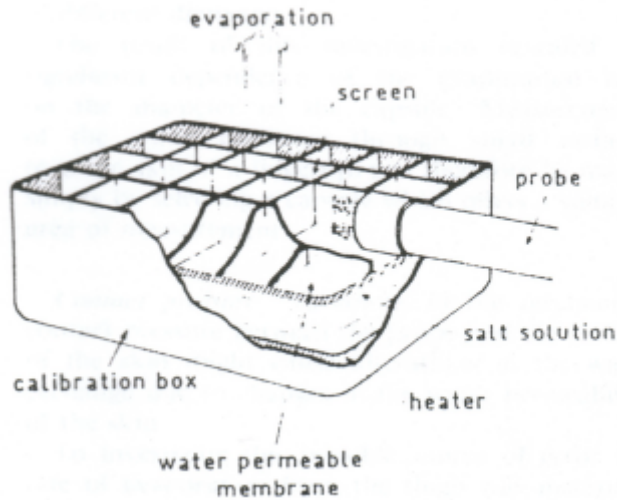


Fig. 12 Correlation between gravimetric loss and measured evaporation rate

Reproduced from:- *Measurement of Water Exchange through Skin*. G E Nilsson, *Med Biol Comput*, 15, 209-18, 1977.

## Membrane TEWL Calibration - Example 2

Petri dish with Opsite membrane

Water temperatures 22-30 °C (up to 80 °C for linearity check)

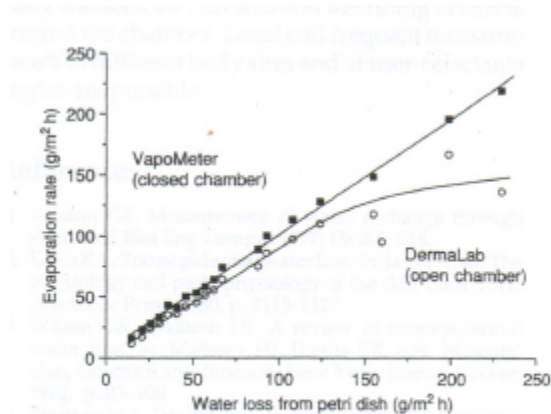


Fig. 3. Evaporation rate using a closed chamber (■) and an open chamber (○) evaporimeter (DermaLab<sup>®</sup>, Cortex Technology, Hadsund, Denmark) vs water loss from the petri dish per unit surface area and time.

Reproduced from:- *A Closed Unventilated Chamber for the Measurement of Transepidermal Water Loss.*  
J Nuutinen, E Alanen, P Autio, M-R Lahtinen, I Harvima & T Lahtinen, *Skin Res & Technol*, 9, 85-9, 2003.

# Membrane TEWL Calibration Model

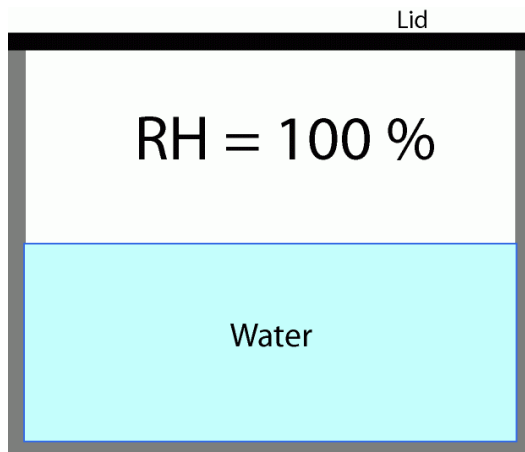
## 1. Closed Cup Vapour/Liquid Equilibrium

Consider a closed cup containing some water:-

For equilibrium, the temperature is uniform everywhere.

For equilibrium, the Relative Humidity (**RH**) of the enclosed air is 100%.

The model uses Vapour Density (Absolute Humidity, Vapour Concentration).



### Note:-

Even in equilibrium at 100% RH, liquid water is **much more dense** than water vapour. Eg at 22°C:-

Water Vapour Density  $\rho_V \sim 0.02 \text{ kg/m}^3$   
Liquid Water Density  $\rho_L \sim 1000 \text{ kg/m}^3$

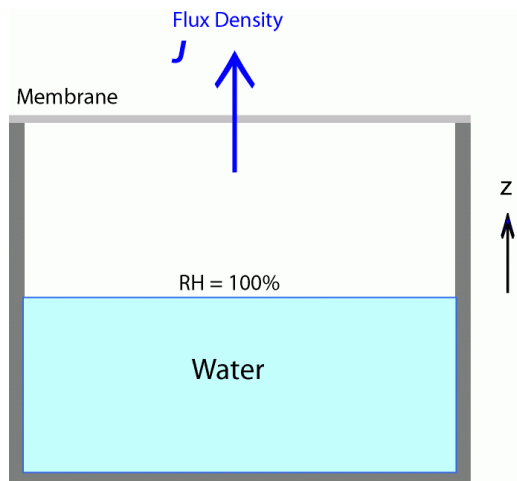
$$\therefore \frac{r_V}{r_L} \approx \frac{1}{50000}$$



# Membrane TEWL Calibration Model

## 2. Leaky Cup Vapour/Liquid Steady-state

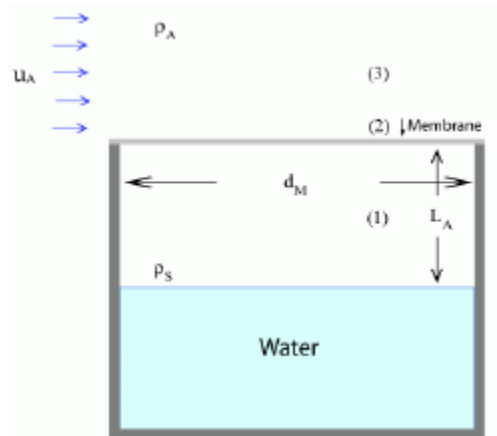
With a permeable lid, there is a flux of water vapour escaping into the ambient air. You no longer have equilibrium, but there can be a steady-state solution, where the flux  $J$  is constant. The RH at the water surface is still 100%, but the humidity falls off towards ambient RH as you move up and away from the water surface.



The question is - how to calculate  $J$ .

# Membrane TEWL Calibration Model

## 3. Flux Calculation for Leaky Cup



Divide the system into three regions:-

**Region 1 (Below the Membrane)**

Diffusion in air, ie Fick's law.

**Region 2 (Within the Membrane)**

Diffusion within the membrane, ie Fick's law.

**Region 3 (Above the Membrane)**

Forced convection. Fick's law within boundary layer.

Join the regions using mass conservation.

# Membrane TEWL Calibration Model

## 4. Fick meets Ohm - the Electrical Analogy

Fick's law can be re-cast as follows:-

$$I = JA = -AD_{VA} \frac{\partial r}{\partial z} = -A D_{VA} \frac{\Delta r}{\Delta z} = -\frac{\Delta r}{R}$$

where  $I = JA$  is the **Flux**  
 $A$  is the cross-sectional **Area**  
 $D_{VA}$  is the **Mass Diffusion Coefficient**  
 $R = Dz/AD_{VA}$  is the **Diffusion Resistance**

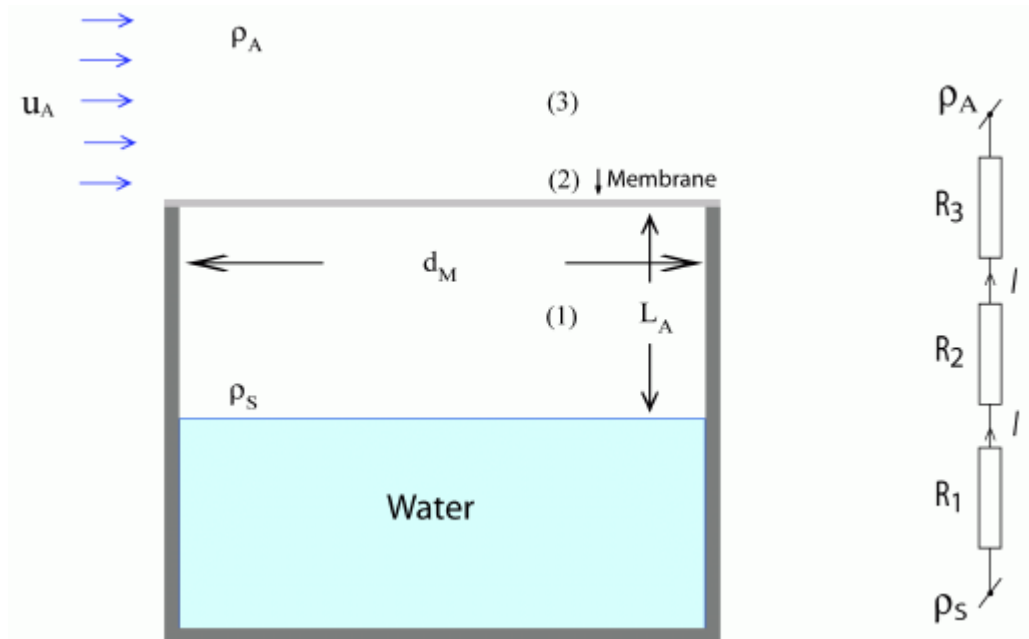
Then, by analogy (see Wheldon & Monteith<sup>1</sup>, for example):-

$I$  is analogous to **electrical current**  
 $Dr$  is analogous to **potential difference**  
 $R$  is analogous to **electrical resistance**

The analogy is useful, because you can use circuit theory to simplify the solution of complex problems.

# Membrane TEWL Calibration Model

## 5. Electrical Equivalent of Leaky Cup



# Membrane TEWL Calibration Model

## 6. Model Parameters

Ambient temperature:- 21 °C

Ambient RH 50 %

Membrane diameter 100 mm

Membrane-liquid separation 25 mm

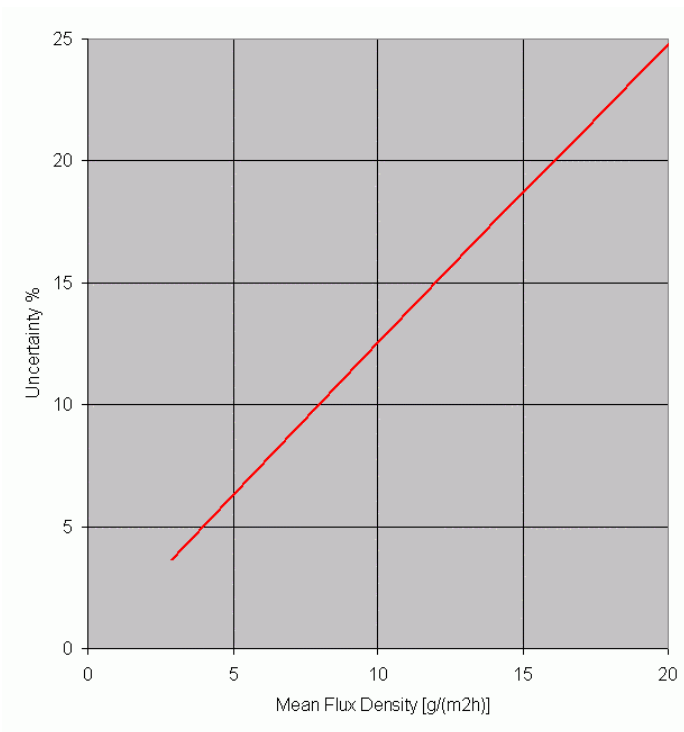
Ambient air movement 0.02 - 0.3 ms<sup>-1</sup>

∴ Ambient boundary layer 13.4 - 3.6 mm

NB:- These conditions are compatible with ASTM-96.

# Membrane TEWL Calibration Model

## Result 1:- Flux Uncertainty caused by Ambient Air Movement

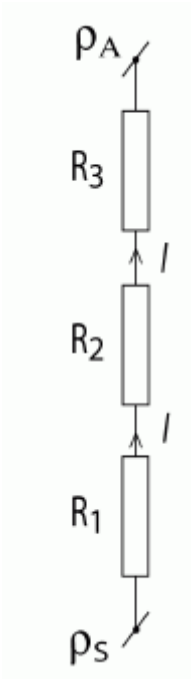


Note:-

1. The uncertainty is small for the low flux levels envisaged in ASTM-96.
2. The uncertainty is significant for the flux levels appropriate for TEWL calibration.

# Membrane TEWL Calibration Model

**Numerical Example:- Diffusion resistances at  $J = 10 \text{ gm}^{-2}\text{h}^{-1}$**



Open Air Boundary Resistance

$R_3 \sim 35 \pm 20$  (arb)

Membrane Resistance

$R_2 \sim 200$  (arb)

Enclosed Air Resistance

$R_1 \sim 100$  (arb)

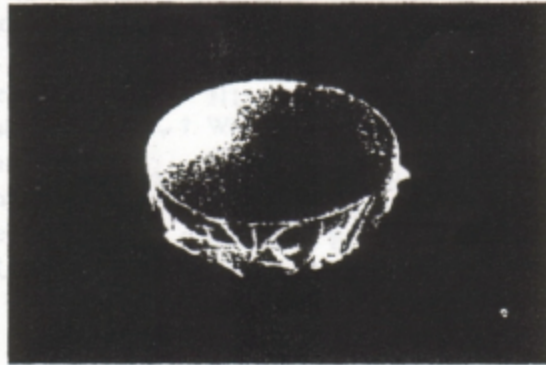
The trouble is that all three resistances are significant.

For constant flux, you need

$$(R_1 + R_2) \gg R_3$$

# Constant Water Evaporation Device

Petri dish with Opsite membrane



*Fig. 6. The constant water evaporation device. See the Section. "Intra- and inter-instrumental variability" and Table 2.*

This device cannot be relied upon to provide a constant flux for TEWL calibration.

Reproduced from:- *Guidelines for Transepidermal Water Loss (TEWL) Measurement*.  
J Pinnagoda, R A Tupker, T Agner & J Serup, *Contact Dermatitis*, 22, 164-78, 1990.



# Membrane TEWL Calibration Model

## Open-chamber Modelling

Cylinder length 20 mm

Cylinder diameter 10 mm

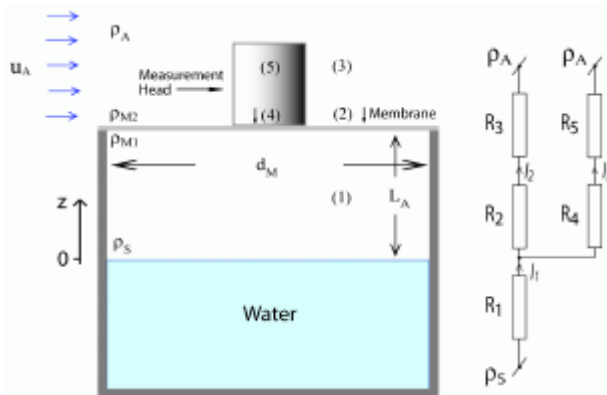
Notes:-

1. Wheldon & Monteith's open-chamber model<sup>1</sup> was used.
2. The effects from centrally placed sensors and foam pads have not been taken into account. These cause the diffusion resistance of the measurement head to increase.
3. The ambient and other conditions are as before.

<sup>1</sup> A E Wheldon & J L Monteith, *Performance of a Skin Evaporimeter*, Med Biol Comput, 18, 201-5, 1980.

# Membrane TEWL Calibration Model

## Result 2:- TEWL Calibration Method 1 (Exposed Membrane)



You now have two additional regions:-

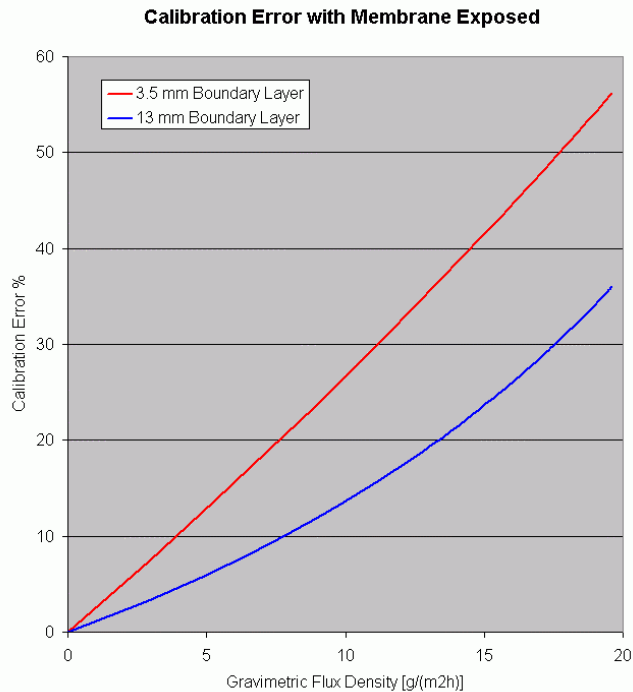
**Region 4** (Membrane under Measurement Head)  
Diffusion within the membrane, ie Fick's law.

**Region 5** (Measurement Head)  
Diffusion in air, ie Fick's law.

In general, the flux densities in the two branches will not be equal.

# Membrane TEWL Calibration Model

## Result 2:- Method 1 Calibration Error (Exposed Membrane)



Calibration Error calculated from:-

$$e = 100 \cdot \frac{J_G - J_H}{J_G}$$

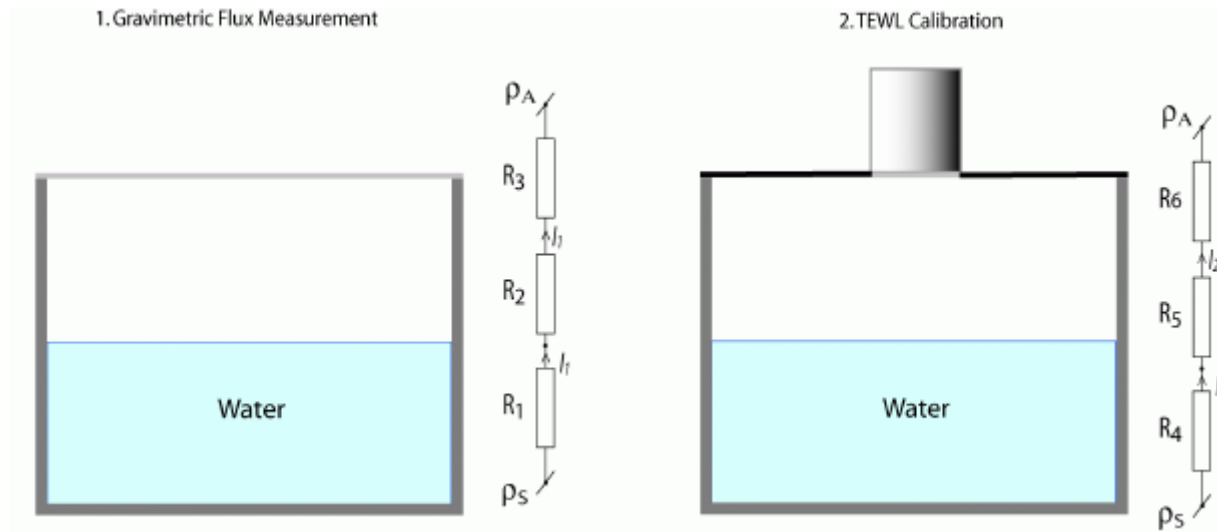
where

$J_G$  = Gravimetric Flux Density

$J_H$  = Measurement Head Flux Density

# Membrane TEWL Calibration Model

## Result 3:- TEWL Calibration Method 2 (Covered Membrane)

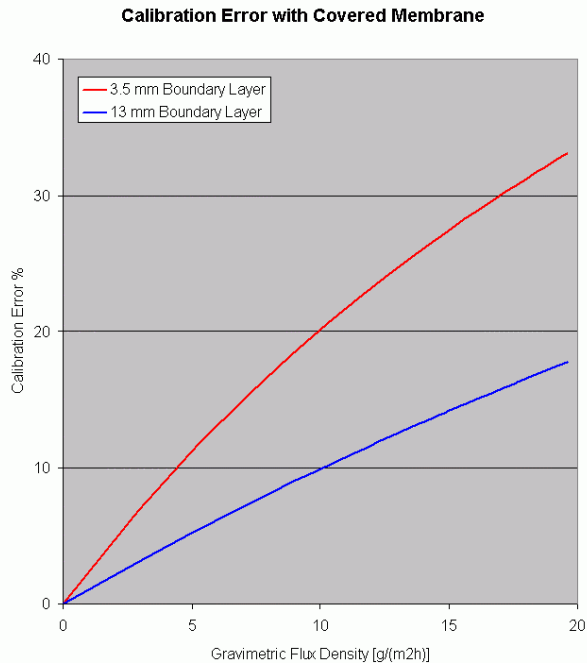


Gravimetric measurement of Flux  
Density from cup weight loss. You  
need a large membrane area for this.

Calibration of TEWL instrument  
with the membrane outwith the  
measurement head covered.

# Membrane TEWL Calibration Model

## Result 3:- Method 1 Calibration Error (Covered Membrane)



Calibration Error calculated from:-

$$e = 100 \cdot \frac{J_G - J_H}{J_G}$$

where

$J_G$  = Gravimetric Flux Density

$J_H$  = Measurement Head Flux Density

## Conclusions

The Cup + Membrane system is NOT a constant flux device for TEWL Calibration.

Gravimetric flux density is NOT equal to Measurement Head flux density .

Therefore, ASTM-96 is NOT a good starting point for a reliable calibration.

# Acknowledgements

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